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# Partial oxidation of methane over Ni/Ce-Ti-O catalysts

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## **Abstract**

Partial oxidation of methane (POM) was studied in this work. The supported nickel catalysts were prepared by the coprecipitation–impregnation method. The influence of the molar ratio of Ce/Ti, the calcination temperature, and the content of active component were investigated during the process of preparation. The results show that the mixed oxides of the Ce-Ti-O-supported Ni catalysts exhibited high catalytic activity and stability. Among the catalysts investigated, the highest catalytic activity was observed over  $10 \text{ wt}\%$  NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-700 °C which showed excellently stable performance during 100 h on stream at 750 °C. The catalysts were characterized by DTA/TG, BET, XRD, and TPR. XRD and TPR results confirmed that the NiO in all catalysts was highly dispersed. There was no NiO but only NiTiO<sub>3</sub> in the NiO/TiO<sub>2</sub> catalyst, due to the reaction between NiO and TiO<sub>2</sub>. NiTiO<sub>3</sub> is harder to be reduced to Ni<sup>0</sup> than NiO. The addition of CeO<sub>2</sub> could form a solid solution of Ce-Ti-O, which was able to restrain the reaction between NiO and TiO<sub>2</sub> and improve the storage capacity and mobility of oxygen. It was shown that  $Ni<sup>0</sup>$  reduced from  $NiTiO<sub>3</sub>$  was active for the POM reaction.

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*Keywords:* Partial oxidation of methane; POM; Ceria; Titania; Solid solution; Hydrogen production

## **1. Introduction**

In recent years, fuel cells have received a great deal of attention [\[1\],](#page-8-0) particularly from the automotive industry [\[2\].](#page-8-0) Proton exchange membrane fuel cell (PEMFC), as a candidate for near-future power generation applications, is particularly suited to automotive applications primarily because its relatively low operating temperature, efficiency, and high power density make it comparable to existing internal combustion technology [\[3\].](#page-8-0)

Hydrogen resource is an important system in PEMFC. There are many routes for hydrogen production [\[4\].](#page-8-0) As a result of various difficulties for hydrogen storage, more attention has been paid to on-board hydrogen production. Partial oxidation of methane (POM) is a suitable hydrogen production process [\[5\]](#page-8-0) because it has rapid reaction velocity, low consumption of energy, and low investment.

The catalyst design is the main point for the POM process. Two groups of catalysts have been studied for partial oxidation of methane: noble metal-based catalysts and Ni-based catalysts. The former includes Pt [\[6\],](#page-8-0) Pd [\[7\],](#page-8-0) Rh [\[8,9\],](#page-8-0) Ru [\[10\]](#page-8-0) and Ir

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[\[11\],](#page-8-0) and Rh and Ru have the highest activity and stability [\[12\].](#page-8-0) Noble metal-based catalysts seem to be more active for the POM reaction than Ni-based catalysts, but the high-cost limits their industrial utilization.

Ni-based catalysts have been investigated for several years [\[13–18\]](#page-8-0) because of their appreciable catalytic activity, good stability, and low price. Since the support can exert a great influence on the type of carbonaceous species formed by the methane interaction with the metallic particles dispersed on its surface, it has an intense effect on catalyst performance. The usual supports include oxides such as  $Al_2O_3$ , MgO, SiO<sub>2</sub>, CaO, Y<sub>2</sub>O<sub>3</sub>, La<sub>2</sub>O<sub>3</sub>, ZrO<sub>2</sub>, CeO<sub>2</sub>, TiO<sub>2</sub>, HfO<sub>2</sub>, MgMAlO<sub>x</sub> spinel, CaTiO<sub>3</sub> perovskite, H-Y zeolite, and their mixed oxides [\[13\].](#page-8-0) Diskin et al. [\[14\]](#page-8-0) prepared supported-Ni catalysts with different supports.  $Ni/SiO<sub>2</sub>$  showed the highest activity and selectivity for CO formation,  $Ni/Al<sub>2</sub>O<sub>3</sub>$  the worst. Wu et al. [\[15\]](#page-8-0) investigated the deactivation of methane to syngas over the  $Ni/TiO<sub>2</sub>$  catalyst. They found that deactivation is due largely to the oxidation of  $Ni<sup>0</sup>$ to NiTiO<sub>3</sub> rather than by carbon deposition in the POM reaction. Zhu and Flytzani-Stephanopoulos [\[16\]](#page-8-0) synthesized the bulk Ni- $CeO<sub>2</sub>$  catalysts by the urea coprecipitation method using metal nitrates and urea. The results confirmed that  $5$  at.% Ni-CeO<sub>2</sub> catalyst showed excellent resistance to carbon deposition and stable performance during 100 h-on-stream at 650 ◦C. Mixed oxidessupported catalysts often show great performance. Roh et al. [\[17\]](#page-8-0) prepared several catalysts for the POM reaction. They found that Ni/Ce-ZrO<sub>2</sub> catalyst had higher activity than Ni/CeO<sub>2</sub> or Ni/ZrO2. They explained that the presence of ceria in the catalyst had beneficial effects on enhancing the concentration of highly mobile oxygen species and the ceria-zirconium solid solution led to a lower reduction temperature. Takeguchi et al. [\[18\]](#page-8-0) discovered the activity of the  $NiO/CeO<sub>2</sub>-ZrO<sub>2</sub>$  catalysts increased with an increase of oxygen storage capacity of the  $CeO<sub>2</sub>-ZrO<sub>2</sub>$  solid solutions. The NiO particles having strong interaction with the support showed high stability for partial oxidation of methane, while the NiO particles having weak interaction produced a large amount of coke.

CeO2, a stable fluorite-type oxide, has a good oxygen storage capacity [\[19\].](#page-8-0) It can be reduced in oxygen deficient conditions while oxidized in oxygen sufficient conditions. Ceria has been examined as a promoter of both the activity and selectivity of Ni catalysts for the POM reaction [\[20\]. T](#page-8-0)itanium and zirconium are both IVB elements, and  $Ti^{4+}$  has a smaller ionic radius than  $Zr^{4+}$ . That indicates it may have great effect on the mobile oxygen species after  $Ti^{4+}$  gets into the ceria crystal lattice. Researchers have discovered that ceria-titania compound oxides have special redox behavior [\[21,22\].](#page-8-0) They were used in supported-CuO catalysts [\[23\].](#page-8-0)

Among Ni-based catalysts,  $NiO/CeO<sub>2</sub>-TiO<sub>2</sub>$  compound oxides catalysts have been rarely reported. In this work, we have studied a  $CeO<sub>2</sub>-TiO<sub>2</sub>$ -supported Ni catalyst for POM, and it is found that the active component in  $Ni/CeO<sub>2</sub>-TiO<sub>2</sub>$  and  $Ni/CeO<sub>2</sub> ZrO<sub>2</sub>$  is different.

# **2. Experimental**

## *2.1. Catalyst preparation*

The compound oxide supports were prepared by coprecipitation. 0.5 mol L<sup>-1</sup> Ce(NO<sub>3</sub>)<sub>3</sub> solution and 0.3 mol L<sup>-1</sup> TiCL<sub>4</sub> solution were mixed in proportion. The mixed solution and  $2 \text{ mol} L^{-1}$  ammonia were dropped together while stirring vigorously and maintained at pH 10, aging for 24 h after the reaction. The precipitate was washed three times with 200 mL deionized water and twice with 100 mL ethanol, and then dried in an oven at 80 ◦C for 24 h, producing a precursor. The supported-Ni catalyst was prepared by impregnating the precursor with an aqueous solution of  $Ni(NO<sub>3</sub>)<sub>2</sub>$ . It was deposited overnight to disperse it well, then dried in an oven at  $80^{\circ}$ C for 24 h again. This was followed by pre-calcining in air at 350 ◦C for 2 h, then at a proper temperature for 4 h.

The expression of catalyst stands for, taking  $10 \text{ wt.} %$ NiO/Ce $_{0.50}$ Ti $_{0.50}$ O<sub>2</sub>-800 °C as an example, the catalyst with a NiO content is 10 wt.%, a molar ratio of Ce/Ti is 0.50:0.50, and calcined at 800 ◦C.

## *2.2. Catalytic reaction*

Catalytic activity tests were carried out in a fixed tubular quartz micro-reactor (500 mm length, 8 mm i.d.) operated at atmospheric pressure. A 100 mg catalyst sample was used for all runs. Catalyst was first reduced in 5 vol.% H<sub>2</sub>–Ar at 650 °C for 30 min. Then the reactor system was flushed in nitrogen for 10 min. The reactant gas of 16 vol.% CH<sub>4</sub>, 10 vol.%  $O_2$  in nitrogen was then introduced to the reactor.  $O_2$  was taken in slight excess over the stoichiometry to compensate its deficiency caused by total combustion. Gas flow rates were controlled at GHSV = 55,200 mL  $h^{-1}$   $g_{cat}^{-1}$  by mass flow meters. The reactant and product mixtures were analyzed by a SP-2100 gas chromatograph (GC) equipped with a thermal conductivity detector and two columns. A carbon sieve GDX-502 (packed column, 2 m length, 4 mm i.d.) column was used to separate  $CO<sub>2</sub>$  and other gases  $(O_2, N_2, CO,$  and  $CH_4)$  while a molecular sieve 5A column was used to separate  $O_2$ ,  $N_2$ , CO, and CH<sub>4</sub>. Conversion of methane and selectivity of carbon monoxide and hydrogen are calculated by the following formulae:

$$
X(CH_4) = \frac{(CH_4)_{in} - (CH_4)_{out}}{(CH_4)_{in}} \times 100\%
$$
 (1)

$$
S(CO) = \frac{(CO)_{out}}{(CH_4)_{in} - (CH_4)_{out}} \times 100\%
$$
 (2)

$$
S(H_2) = \frac{(H_2)_{\text{out}}}{2[(CH_4)_{\text{in}} - (CH_4)_{\text{out}}]} \times 100\%
$$
 (3)

### *2.3. Characterization technique*

Specific surface areas were calculated by the BET method from  $N_2$  adsorption isotherms, recorded at liquid nitrogen temperature on a Micromeritics apparatus model ASAP-2000.

Powder X-ray diffraction (XRD) patterns of samples were recorded on D/Max-2500 X-ray diffractometer in order to identify the different phases present in the catalyst and to determine their crystalline phases. Cu K $\alpha$  radiation ( $\lambda = 0.15406$  nm) was used with a power setting of  $40 \text{ kV}$  and  $100 \text{ mA}$ . (scan rate =  $5^\circ$  min<sup>-1</sup>).

Temperature programmed reduction (TPR) of the samples was carried out in a TPR analyzer (Thermo Finnigan modeled TPDRO 1100 Series) in a 5 vol.%  $H_2-N_2$  gas mixture with a rate of 20 mL min−1. A 10 mg catalyst sample was used in each run. After being loaded into the quartz tube reactor, the sample was heated in the gas mixture from room temperature to 950 °C with a heating rate of  $10^{\circ}$ C min<sup>-1</sup>, and then maintained at 950 °C for 5 min.

Differential thermal analysis and thermo gravimetric analysis (DTA/TG, Perkin-Elmer, Pyris Diamond) were made in a dry-air atmosphere using a heating rate of  $10^{\circ}$ C min<sup>-1</sup>.

## **3. Results and discussion**

#### *3.1. BET surface area results*

[Table 1](#page-2-0) gives the specific surface areas of catalysts prepared in various conditions. According to [Table 1, t](#page-2-0)he specific surface areas increase with the addition of ceria, and decrease with an increase in calcination temperature and with an increase in Ni content.

<span id="page-2-0"></span>Table 1 BET surface area of different catalysts

Catalyst	BET surface area $(m^2 g^{-1})$
10 wt.% NiO/TiO2-800 °C	4.0
10 wt.% NiO/Ce <sub>0.25</sub> Ti <sub>0.75</sub> O <sub>2</sub> -800 °C	15.1
10 wt.% NiO/Ce <sub>0.50</sub> Ti <sub>0.50</sub> O <sub>2</sub> -800 °C	19.2
10 wt.% NiO/Ce <sub>0.75</sub> Ti <sub>0.25</sub> O <sub>2</sub> -800 °C	17.1
10 wt.% NiO/CeO <sub>2</sub> -800 °C	28.1
10 wt.% NiO/Ce <sub>0.50</sub> Ce <sub>0.50</sub> Ti <sub>0.50</sub> O <sub>2</sub> -700 °C	37.2
10 wt.% NiO/Ce <sub>0.50</sub> Ti <sub>0.50</sub> O <sub>2</sub> -900 °C	11.3
5 wt.% NiO/Ce <sub>0.50</sub> Ti <sub>0.50</sub> O <sub>2</sub> -800 °C	23.5
15 wt.% NiO/Ce <sub>0.50</sub> Ti <sub>0.50</sub> O <sub>2</sub> -800 °C	18.6

## *3.2. Catalytic performance*

The catalytic performance of the catalysts is influenced by their preparation conditions. The molar ratio of Ce/Ti, the calcination temperature, and the content of Ni are essential parameters that should be controlled.

#### *3.2.1. Effect of Ce/Ti ratio*

10 wt.% NiO/Ce*x*Ti1−*<sup>x</sup>*O2 samples with different Ce/Ti ratios  $(x=0, 0.25, 0.50, 0.75, 1)$  were prepared. The five catalysts were all active for the POM reaction with similar trends, as shown in Fig. 1. Conversion of CH4 was enhanced at hightemperature and kept going up as the temperature rose. 10 wt.% NiO/Ce $_{0.50}$ Ti $_{0.50}$ O<sub>2</sub>-800 °C exhibited the highest CH<sub>4</sub> conversion at the reaction temperature range of  $700-800$  °C. CH<sub>4</sub> conversion reached 95% at 800 ◦C, which is close to the equilibrium conversion. Table 1 shows that  $10 \text{ wt. } \%$  NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 had the largest specific surface area among the three  $Ce<sub>x</sub>Ti<sub>1-x</sub>O<sub>2</sub>$ -supported catalysts, which indicates that the high activity might be partly the result of its high specific surface area.

#### *3.2.2. Effect of calcination temperature*

10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub> catalysts were calcined at 700, 800, and  $900^{\circ}$ C. The catalytic activity decreases with an increase in calcination temperature, as shown in [Fig. 2.](#page-3-0) Especially at lower reaction temperature (650 $\degree$ C), CH<sub>4</sub> conversion is 82% over catalyst calcined at 700  $\degree$ C, while only 76 and 75% over catalysts calcined at 800 and 900 ◦C, respectively. The results in Table 1 also show that catalyst calcined at 700 ◦C has the largest BET surface area. The small surface area of catalysts calcined at high-temperature may lead to lower  $CH<sub>4</sub>$  conversion. Meanwhile, high calcination temperature might result in separation of  $TiO<sub>2</sub>$  from Ce-Ti solid solution (this will be discussed in Section [3.4\),](#page-4-0) which may also influences the catalytic performance.

#### *3.2.3. Effect of Ni content*

Catalysts with NiO loading of 5, 10, and 15 wt.% were prepared by impregnating  $Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>$  with  $Ni(NO<sub>3</sub>)<sub>2</sub>$ . [Fig. 3](#page-3-0) lists the results of catalytic performance measurement. As shown in [Fig. 3\(a](#page-3-0)), CH4 conversion increases by 4 and 8% at 650 and 700 $\degree$ C, respectively with the NiO content increasing from 5 to 10 wt.%. When NiO loading is higher than  $10$  wt.%, CH<sub>4</sub> con-



Fig. 1. Catalytic activity of 10 wt.% NiO/Ce<sub>*x*</sub>Ti<sub>1−*x*</sub>O<sub>2</sub>-800 °C with different Ce/Ti: (a) CH4 conversion-temperature, (b) CO selectivity-temperature and (c) H<sub>2</sub> selectivity-temperature (( $\blacksquare$ )10 wt.% NiO/TiO<sub>2</sub>-800 °C; ( $\blacksquare$ ) 10 wt.% NiO/Ce<sub>0.25</sub>Ti<sub>0.75</sub>O<sub>2</sub>-800 °C; (▲) 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C; (▼) 10 wt.% NiO/Ce<sub>0.75</sub>Ti<sub>0.25</sub>O<sub>2</sub>-800 °C; and ( $\blacklozenge$ ) 10 wt.% NiO/CeO<sub>2</sub>-800 °C).

<span id="page-3-0"></span>version shows a slight decrease at the reaction temperature of 650 and 700 $\degree$ C. So 10 wt.% NiO loading is sufficient, more NiO has little contribution to catalytic activity for the POM reaction.

## *3.3. Stability testing results*

The 10 wt.% NiO/Ce $_{0.50}$ Ti $_{0.50}$ O<sub>2</sub>-700 °C catalyst showed a very good stability at 750 °C with a CH<sub>4</sub>/O<sub>2</sub> ratio of 1.6 at a GHSV of 55,200 mL  $h^{-1}$   $g_{cat}^{-1}$ , as shown in [Fig. 4.](#page-4-0) No distinct



Fig. 2. Catalytic activity of 10 wt.%  $NiO/Ce_{0.50}Ti_{0.50}O_2$  calcined at different temperature: (a) CH4 conversion-temperature, (b) CO selectivity-temperature and (c) H<sub>2</sub> selectivity-temperature (( $\blacksquare$ ) 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-700 °C; (●) 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C; and (▲) 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>- $900\,^{\circ}\mathrm{C}$ ).



Fig. 3. Catalytic activity of NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C with different NiO content: (a) CH<sub>4</sub> conversion-temperature, (b) CO selectivity-temperature and (c)  $H_2$ selectivity-temperature (( $\blacksquare$ ) 5 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C; ( $\blacksquare$ ) 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C; and ( $\triangle$ ) 15 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C).

<span id="page-4-0"></span>

Fig. 4. Stability test of 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0</sub>.<sub>50</sub>O<sub>2</sub>-700 °C at 750 °C, GHSV = 55,200 mL h<sup>-1</sup>  $g_{cat}^{-1}$  and CH<sub>4</sub>:O<sub>2</sub> = 1.6:1 ((■) conversion of CH<sub>4</sub>; (●) selectivity of CO; and  $(\triangle)$  selectivity of H<sub>2</sub>).

deactivation was observed during 100h on stream. CH<sub>4</sub> conversion and H2 selectivity were maintained at ∼93 and ∼90%, respectively.

From the catalytic performance tests, we could found that the Ni/Ce-Ti-O catalysts had excellent activity and stability for the POM reaction. Wu et al. [\[15\]](#page-8-0) prepared supported  $Ni/TiO<sub>2</sub>$  catalyst, and it exhibited rapid deactivation from the start in the POM process. It indicates that the addition of ceria greatly improves the resistance to deactivation. Table 2 lists the comparison of

#### Table 2

Comparison of catalytic activity of different catalysts for POM reaction

catalytic activity of different catalysts in the literatures and this work. This implies that Ni/Ce-Ti-O is a potential catalyst for the POM reaction.

# *3.4. XRD results*

XRD studies were performed on the calcined samples prepared in different conditions. For discerning the structure more clearly, the crystalline phases involved in each catalyst are summarized in Table 3, and Table 3 also shows the ceria lattice parameter calculated from ceria (1 1 1) reflection. [Figs. 5–7](#page-5-0) depicts the XRD patterns of all samples.

XRD patterns for catalysts with different Ce/Ti ratios are shown in [Fig. 5\(A](#page-5-0)–E). Discernible NiO diffraction peaks were only found in the  $NiO/CeO<sub>2</sub>$  sample. This indicates that no bulk  $NiO$  exists in the other catalysts. NiTiO<sub>3</sub> diffraction peaks were clearly observed in all catalysts except  $NiO/CeO<sub>2</sub>$ . That is to say, TiO2 addition avoids the formation of bulk NiO due to the solidstate reaction of NiO and TiO<sub>2</sub>. No obvious TiO<sub>2</sub> diffraction peaks appeared in the NiO/Ce<sub>0</sub>.75Ti<sub>0</sub>.25O<sub>2</sub> catalysts. The CeO<sub>2</sub> lattice parameter in NiO/Ce-Ti-O decreases compared with that in NiO/CeO<sub>2</sub>, as shown in Table 3. Ti<sup>4+</sup> has a smaller ionic radius than  $Ce^{4+}$ . After Ti<sup>4+</sup> enters the ceria crystal lattice, the  $CeO<sub>2</sub>$  lattice parameter should decrease. It can be seen from Table 3 that the  $CeO<sub>2</sub>$  lattice parameter is smaller in NiO/Ce-Ti-O compared with in NiO/CeO<sub>2</sub>, which indicates the formation of ceria-titania solid solution. So, the smaller ceria lattice parameter, the more  $Ti<sup>4+</sup>$  enters the ceria crystal lattice, the more ceria-titania solid solution forms. By combining this XRD study with the results



Table 3

The crystalline phases and ceria lattice parameter in each catalysts



<sup>a</sup> Calculated from ceria (1 1 1) reflection from the equation  $a = \sqrt{h^2 + k^2 + l^2} (\lambda/2 \sin \theta)$  [\[24\].](#page-8-0)

<span id="page-5-0"></span>

Fig. 5. XRD patterns of 10 wt.% NiO/Ce<sub>*x*</sub>Ti<sub>1−*x*</sub>O<sub>2</sub>-800 °C with different Ce/Ti ratio: (A) 10 wt.% NiO/TiO<sub>2</sub>-800 °C; (B) 10 wt.% NiO/Ce<sub>0.25</sub>Ti<sub>0.75</sub>O<sub>2</sub>-800 °C; (C)  $10 \text{ wt. } \%$  NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C; (D)  $10 \text{ wt. } \%$  NiO/Ce<sub>0.75</sub>Ti<sub>0.25</sub>O<sub>2</sub>-800 °C; and (E) 10 wt.% NiO/CeO<sub>2</sub>-800 °C.

of the catalytic activity tests, it is found that the best catalyst, 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-700 °C, has the smallest ceria lattice parameter, which indicates that the correlation of ceriatitania solid solution and the catalytic activity.

Fig.  $6(A-C)$  lists the XRD patterns of 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub> calcined at 700, 800, and 900 °C. All diffraction peaks become shaper with the increase of calcination temperature. No obvious  $TiO<sub>2</sub>$  diffraction is present in the catalysts calcined at 700 ◦C, which shows that titanium is in the form of Ce-Ti-O solid solution and  $NiTiO<sub>3</sub>$ . Rutile diffraction peaks are observed in catalysts calcined 800 and 900 ◦C. The results imply that the ceria-titania solid solution was not very stable, and titania would separate out at higher calcination temperatures. As shown in [Fig. 2,](#page-3-0) catalyst calcined at 700 ◦C exhibited a higher activity than at 800 or 900 ℃ in POM.



Fig. 6. XRD patterns of  $10 \text{ wt.} %$  NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub> calcined at different temperature: (A) 10 wt.% NiO-Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-700 °C; (B) 10 wt.% NiO- $Ce_{0.50}Ti_{0.50}O_2$ -800 °C; and (C) 10 wt.% NiO- $Ce_{0.50}Ti_{0.50}O_2$ -900 °C.



Fig. 7. XRD patterns of NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C with different NiO content: (A) 5 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C; (B) 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C; and (C) 15 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C.

Thus, catalytic performance may be related to the formation of ceria-titania solid solution to some extent.

Fig. 7(A–C) shows the XRD patterns of NiO/  $Ce<sub>0.50</sub>$  oTi<sub>0.50</sub>O<sub>2</sub>-800 °C catalysts with NiO content of 5, 10, and 15 wt.%. TiO<sub>2</sub> diffraction peaks become weaker, while  $NiTiO<sub>3</sub>$  diffraction peaks become stronger with the increase of NiO loading. This means the solid-state reaction of NiO and  $TiO<sub>2</sub>$  is improved by the increase of NiO content.

# *3.5. TPR results*

The reduction behavior of Ni-based catalysts was investigated by means of TPR. All catalysts were examined in 5 vol.% H<sub>2</sub> in N<sub>2</sub>. TPR profiles of 10 wt.% NiO/Ce<sub>x</sub>Ti<sub>1−*x*</sub>O<sub>2</sub>-800 °C with different Ce/Ti ratios are shown in [Fig. 8\(A](#page-6-0)–E). Only one reduction peak is observed in NiO/TiO<sub>2</sub> at about 630 °C, which is due to the reduction of  $Ni^+$  in bulk NiTiO<sub>3</sub> to Ni<sup>0</sup> [\[15\].](#page-8-0) At least three reduction peaks are observed for  $NiO/CeO<sub>2</sub>$  at temperatures of 280, 380, and 790 ◦C. Unsupported NiO has a reduction temperature of about  $280^{\circ}$ C [\[15\].](#page-8-0) Therefore, the small peak between 260 and 300 °C in NiO/CeO<sub>2</sub> is assigned to bulk NiO. The peak at the temperature of about  $380^{\circ}$ C is due to the reduction of NiO interacted with the support[\[15,18,25\]. T](#page-8-0)he small and broad peak at 790 °C is related to the partial reduction of  $Ce^{4+}$  to  $Ce^{3+}$  [\[15,26,27\]. T](#page-8-0)hree obvious reduction peaks are presented in the other three  $Ce<sub>x</sub>Ti<sub>1-x</sub>O<sub>2</sub>$ -supported catalysts at temperatures of 390, 650, and 800 °C. The reduction peaks near 390 °C are exhibited in [Fig. 8\(B](#page-6-0)–E), which is due to the reduction of NiO interacting with support, while no NiO diffraction peaks can be detected for the same samples in the XRD patterns. It indicates that NiO species are highly dispersed in these catalysts.

Though only the  $NiTiO<sub>3</sub>$  reduction peak presented itself in NiO/TiO<sub>2</sub>, a high catalytic activity was shown over the catalysts. This shows that  $Ni<sup>0</sup>$  reduced from NiTiO<sub>3</sub> species could be active to the POM reaction. Wu et al. [\[15\]](#page-8-0) studied the deactivation of  $Ni/TiO<sub>2</sub>$  catalyst. Rapid deactivation was observed from the

<span id="page-6-0"></span>

Fig. 8. TPR profiles of 10 wt.% NiO/Ce<sub>x</sub>Ti<sub>1−*x*</sub>O<sub>2</sub>-800 °C with different Ce/Ti ratio: (A) 10 wt.% NiO/TiO<sub>2</sub>-800 °C; (B) 10 wt.% NiO/Ce<sub>0.25</sub>Ti<sub>0.75</sub>O<sub>2</sub>-800 °C; (C)  $10 \text{ wt. } \%$  NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C; (D)  $10 \text{ wt. } \%$  NiO/Ce<sub>0.75</sub>Ti<sub>0.25</sub>O<sub>2</sub>-800 °C; and (E) 10 wt.% NiO/CeO<sub>2</sub>-800 °C.

start in the POM process. CH<sub>4</sub> conversion decreased from an initial value of 76–43% after 20 h of reaction. They concluded that the formation of  $NiTiO<sub>3</sub>$  was the main reason for catalysts deactivation. That is different from our conclusion. Despite the hard reduction of NiTiO<sub>3</sub>, the Ni<sup>0</sup> reduced from NiTiO<sub>3</sub> is still an active component for POM reaction.

Fig. 9(A–C) presents TPR profiles of  $10 \text{ wt.} %$ NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub> calcined at 700, 800, and 900 °C. At least three reduction peaks are observed for all catalysts at temperatures of about 390, 650, and 800 ◦C. The reduction peaks at about 390 ◦C become weaker as the calcination temperature of catalysts increase. This suggests that NiO interaction with the support was not stable, and the solid-state reaction between NiO and  $TiO<sub>2</sub>$  are improved as calcination temperature increases. Comparing these three TPR profiles, from A to C, the reduction



Fig. 9. TPR pattern of  $10 \text{ wt.} %$  NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub> calcined at different temperature: (A)  $10 \text{ wt. } \%$  NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-700 °C; (B) 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C; and (C) 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-900 °C.



Fig. 10. TPR profiles of NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C with different NiO content: (A) 5 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C; (B) 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C; and (C) 15 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-800 °C.

peak of  $650\degree C$  is shifted to a higher value, which indicates that the higher the calcination temperature, the stabler the NiTiO<sub>3</sub>. There are also a series of weak peaks between 830 and 900 °C. These may be related to the reduction of different types of ceria-titania solid solution.

TPR profiles of NiO/Ce $_{0.50}$ Ti $_{0.50}$ O<sub>2</sub>-800 °C with NiO loading of 5, 10, and 15 wt.% are shown in Fig. 10(A–C). The reduction area of 670 ◦C increases with the increase of NiO loading. This means that the increase of NiO is mainly to forming NiTiO<sub>3</sub>. An unresolved peak with the maximum temperature at  $420^{\circ}$ C is observed in the 15 wt.% NiO catalyst. This suggests that there are two kinds of NiO species. The peak at a lower temperature is assigned to the NiO species interacting weakly with support, and the peak at the higher temperature is attributed to a complex NiO species interacting more strongly with the support [\[28\].](#page-8-0)

TPR measurements of the different supports were executed to determine the use of Ce in improving the storage capacity and mobility of oxygen. Fig. 11 shows the TPR profiles of the



Fig. 11. TPR profiles of the different catalyst supports: (A)  $TiO<sub>2</sub>$ -700 °C; (B)  $CeO<sub>2</sub>-700 °C$ ; (C)  $Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-700 °C$ .

supports, TiO<sub>2</sub>, CeO<sub>2</sub>, and Ce<sub>0.50</sub>T<sub>i0.50</sub>O<sub>2</sub> calcined at 700 °C. No distinct reduction peak was observed in the  $TiO<sub>2</sub>$  support. The reduction profile of  $CeO<sub>2</sub>$  showed two peaks. The first, lowtemperature, signal located at 500 ◦C was assigned to the reduction of surface-capping oxygen of ceria, while removal of the bulk oxygen was suggested as the cause of the high-temperature signal at 750 °C [\[29\].](#page-8-0) And the  $Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>$  presented similar reduction peaks, but both these two peaks shifted to higher temperature. Also, the peak area was larger than for  $CeO<sub>2</sub>$ . The calculated area (per mol of Ce) of the low-temperature peak is 3.7 times larger for  $Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>$  than for  $CeO<sub>2</sub>$ , and the hightemperature peak is 2.5 times larger for  $Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>$  than for  $CeO<sub>2</sub>$ . That is to say, the addition of Ti promotes the reduction of the surface  $CeO<sub>2</sub>$  and bulk  $CeO<sub>2</sub>$ , which can form more bulk oxygen vacancies. The results can help us to confirm that the storage capacity and mobility of oxygen has been improved after the  $Ti^{4+}$  enter the ceria lattice.

At the same time, the  $H_2$  consumption of the reduction peak of ceria is different with the various Ce/Ti in [Fig. 8. A](#page-6-0)ssigning to the peak area of the ceria reduction in  $NiO/CeO<sub>2</sub>$  a value of 1, we calculated the area of this reduction peak (per mol of Ce) in the other catalysts:  $NiO/Ce_{0.75}Ti_{0.25}O_2$  is 1.3,  $NiO/Ce_{0.50}Ti_{0.50}O_2$ is 2.8, and in NiO/Ce<sub>0.25</sub>Ti<sub>0.75</sub>O<sub>2</sub> is 2.0. This means that the storage capacity of oxygen has been improved not only in the support (Ce<sub>0.50</sub>T<sub>i0.50</sub>O<sub>2</sub>), but also in the Ni/Ce-Ti-O catalyst, which is good for resistance to carbon deposition.

## *3.6. DTA/TG results*

As mentioned above, the formation of  $CeO<sub>2</sub>-TiO<sub>2</sub>$  solid solution improved the storage of oxygen. And the oxygen vacancies of the support could resist the carbon deposition [\[30\].](#page-8-0) Information about this aspect was deduced from the thermogravimetric weight gain measurement by comparing measured values with the theoretical weight gain for probable oxidation reaction. DTA/TG analyses of the reduced (fresh catalyst was reduced in 5 vol.% H2–Ar at 650 for 30 min) and used (after 100 h on stream stability testing) 10 wt.% NiO/Ce $_{0.50}$ Ti $_{0.50}$ O<sub>2</sub>-700 °C catalyst were carried out in a dry-air atmosphere using a heating rate of 10 ◦C min−1. Fig. 12 depicts the DTA/TG curves of the samples. There is a broad exothermic peak around 330 ◦C both in the reduced and used catalysts. TG curve of reduced catalyst shows a weight gain of approximately 2%, which is very close to the theoretical weight gain of Ni to NiO, 2.2%. And the reduced temperature (650 $\degree$ C) makes it more reasonable. On the contrary, the used catalyst presents a two steps weight gain, which indicates that some other species have been oxidated. Meanwhile, the total weight gain is 2.9%, so it could not be the oxidation of Ni only. In the used catalyst, besides Ni, there is only  $Ce^{3+}$ could be oxidated, and the oxidation of  $Ce^{3+}$  is easier than Ni. Therefore, we presume that the first step of weight gain (about  $(0.6\%)$  is due to the Ce<sup>3+</sup> to Ce<sup>4+</sup> oxidation; the second step of weight gain (about 2.1%) is due to the  $Ni<sup>0</sup>$  to  $Ni<sup>2+</sup>$  oxidation. Meanwhile, there is no obvious weight loss of carbon in these two samples, which means that there is less or no carbon deposit during 100 h on stream testing. These results imply that there are plenty of oxygen vacancies in the used catalyst, which can resist



Fig. 12. DTA/TG analysis of reduced and used  $10 \text{ wt. } \%$  NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-700 ◦C catalyst.

carbon deposition, and from another point of view, explains the high stability of the catalyst. And it is noticeable that the starting temperature of the second-step weight gain of the used catalyst is 350 °C, which is higher than the reduced one,  $170$  °C. That may be because the sintering of nickel during the high-temperature catalytic performance testing.

Dong et al. [\[31\]](#page-8-0) studied the mechanism over  $Ni/CeO<sub>2</sub>$ ,  $Ni/ZrO<sub>2</sub>$ , and  $Ni/Ce-ZrO<sub>2</sub>$  catalysts. They found that the addition of ceria to zirconia enhanced the activity of the catalyst for CH4 dissociation and improved the carbon storage capacity. Moreover, it increased the storage capacity and mobility of oxygen in the catalyst, thus promoting carbon elimination. Roh et al. [\[17\]](#page-8-0) discovered that the presence of ceria in the Ni/Ce- $ZrO<sub>2</sub>$  catalyst had beneficial effects on the catalyst performance such as improving the catalyst stability and enhancing concentration of the highly mobile oxygen species. And the interaction between zironia and ceria led to the easier reduction of ceria. For the Ni/Ce-TiO<sub>2</sub> catalyst, it is similar to the Ni/Ce-ZrO<sub>2</sub> catalyst in increasing the storage capacity and mobility of oxygen, which promotes the resistance to carbon deposition. But there is a solid-state reaction between NiO and  $TiO<sub>2</sub>$  during the calcination, forming  $NiTiO<sub>3</sub>$  in the fresh catalyst. After being reduced, the  $Ni<sup>0</sup>$  which reduced from NiTiO<sub>3</sub> is the active component for POM reaction. While the active component in  $Ni/Ce-ZrO<sub>2</sub>$  is the  $Ni<sup>0</sup>$  which reduced from the NiO interacted with the support.

## **4. Conclusions**

NiO/Ce-Ti-O catalysts prepared by coprecipitation– impregnation method show a high activity and stability for partial oxidation of methane at the temperature range of 650 to 850 °C. 10 wt.% NiO/Ce<sub>0.50</sub>Ti<sub>0.50</sub>O<sub>2</sub>-700 °C exhibited the highest  $CH_4$  conversion and  $H_2$  selectivity among the catalysts tested, and maintained them during 100 h on stream. XRD and TPR results indicate that the NiO species are well dispersed in the catalysts of NiO/Ce-Ti-O, while bulk NiO particles are just presented in  $NiO/CeO<sub>2</sub>$ . The solid-state reaction between  $TiO<sub>2</sub>$ and NiO is observed in all catalysts containing  $TiO<sub>2</sub>$ , which leads to the formation of  $NiTiO_3$ . The formation of ceria-titania

<span id="page-8-0"></span>solid solution, which might weaken the interaction of NiO and  $TiO<sub>2</sub>$  and have an influence on catalytic stability for the POM reaction, was confirmed by XRD analysis. The solution of  $Ti^{4+}$ into ceria (forming solid solution) elevates the oxygen storage capacity, and improves the resistance to carbon deposition. It is shown that  $Ni^0$  reduced from NiTiO<sub>3</sub> is active for POM.

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